



Wastren-EnergX Mission Support, LLC

P.O. Box 307 • Piketon, OH 45661

DOE Contract No. DE-CI0000004  
PM-14-014  
June 18, 2014

Mr. Johnny Reising, Federal Project Director  
U.S. Department of Energy  
Portsmouth/Paducah Project Office  
P.O. Box 700  
Piketon, OH 45661

**DOE Contract No. DE-CI0000004: 2014 South Fog Road Bridge Inspection Report**

Dear Mr. Reising:

Attached for your review is a copy of the 2014 South Fog Road Bridge Inspection Report, completed by Burgess & Niple, Inc. after their routine inspection of the South Fog Road Bridge on May 29, 2014.

If you have any questions or comments, please contact Chris Ondera, WEMS Deputy Project Manager, at (740) 897-2344.

Sincerely,

A handwritten signature in black ink, appearing to read 'D. Detillion', is written over a horizontal line.

*for* Damon A. Detillion  
Project Manager  
Wastren-EnergX Mission Support, LLC

DAD:CO:sd

Attachment: Inspection Report

c w/attach: Vince Adams, DOE/PPPO  
Joel Bradburne, DOE/PPPO  
Tony Canterbury, WEMS  
Dennis Carr, FBP  
Rick Ginther, FBP  
Jeremy Harley, DOE/PPPO  
Phil Moore, WEMS  
Chris Ondera, WEMS  
File – Project Management  
File – RMDC-RC

# BURGESS & NIPLE

---

5085 Reed Road | Columbus, OH 43220 | 614.459.2050

Mr. Timothy Estrada  
Wastren-EnergX  
Mission Support, LLC  
3930 US 23 South  
Piketon, Ohio 45661

Re: 2014 Inspection of South Fog Road  
Bridge at Piketon Gaseous  
Diffusion Plant

May 23, 2014

Dear Mr. Estrada:

On May 19, 2014, Burgess & Niple, Inc. (B&N) performed a routine inspection of the South Fog Road Bridge located near the Gaseous Diffusion Plant complex near Piketon, Ohio.

The Burgess & Niple inspection team consisted of Dale Poorman, PE and Reed Case, EI. Mark Pelfrey of Wastren-EnergX Mission Support (WEMS) accompanied the inspection team during the field work.

The bridge is located on the Northeast Access Road within the complex which generally runs north-south. A map of the location is shown below. The structure is identified as the South Fog Road Bridge for the purposes of this report. The ODOT Bridge Inspection Field Report form and the DOE NBI Record Data Collection form are included at the end of this report.



Bridge Location

The bridge was inspected according to the *Bridge Inspector's Reference Manual* published by the Federal Highway Administration (FHWA) and the Ohio Department of Transportation (ODOT) *Manual of Bridge Inspection (Revised 2013 v.8)*. This letter report summarizes our findings and recommendations.

The bridge currently is posted with the following load limits:

<u>Truck Configuration</u>	<u>Load Limit</u>
2F1	11 tons
3F1	11 tons
4F1	12 tons
5C1	20 tons

The bridge is rated poor based on the condition of the deck and substructure. The load postings and condition ratings have not changed since the 2013 inspection.



**Photo 1** – Elevation view looking southeast.



**Photo 2 – End view looking south.**

## **SUMMARY OF FINDINGS**

The original South Fog Road Bridge structure consisted of six rolled steel beams and one steel channel (east exterior beam) that spans 34-feet 6-inches over Little Beaver Creek. The steel beams are partially encased in the concrete deck, with corrugated metal pipe arches spanning between the steel beams. No detailed bridge plans or history are available for this portion of the structure. Information supplied by site personnel indicates that the original bridge was most likely constructed in the 1930's. This structure was widened at a later unknown date. The widened portion of the bridge consists of six rolled steel beams supporting a reinforced concrete deck with corrugated metal stay-in-place form. The beams are numbered 1 through 13, from west to east.

### **Deck**

The original bridge deck consists of reinforced concrete which encases the web and top flange of the beams, using half-segments of steel corrugated pipe as forms for the deck (commonly referred to as a jack arch deck). A single layer of reinforcing steel exists in the existing deck. The widened portion of the deck is a 6-inch thick reinforced concrete deck supported by conventional metal stay-in-place forms.

A thin epoxy concrete overlay wearing surface was installed in 2010 on the original portion of the deck to improve the riding surface; however, the new wearing surface has approximately 120 square feet of unsound and spalled epoxy concrete (an increase from 66 square feet in 2013) (Photo 3). The deteriorated wearing surface has exposed 2-inch deep potholes, producing an extremely rough riding surface. This deterioration is possibly the result of chloride contamination of the existing concrete due to application of deicing chemicals over the life of the bridge.

The east exterior 3-1/2 feet of the original deck did not receive the epoxy concrete overlay and still exhibits a full depth hole due to scaling concrete and a large accumulation of deck debris. The full depth hole along the

inside edge of beam 13 measures 26.5-foot long by 17-inch wide (an increase from 23-feet long by 9-inch maximum width in 2011 and 26 feet long by 13-inch maximum width in 2013) (**Photos 4 & 5**). The hole is encroaching into the roadway at this point. This deterioration is common for jack arch decks of this era and is most likely a result of freeze thaw damage from deck drainage penetrating the concrete. The accumulation of debris present along the edge of the roadway will continue to trap water and accelerate the deterioration of the deck. Consideration should be given to replacing the entire original deck. This will not only lengthen the useful life of the structure, but can raise the allowable truck loads, due to the reduction in dead load on the controlling original steel beams. A partial depth deck rehabilitation may result in accelerated deterioration of the existing concrete due to the probable high levels of chlorides in the existing concrete.

Portions of the underside of the concrete deck could not be observed due to stay-in-place forms and corrugated metal pipe covering the widened and original deck portions, respectively. Surface corrosion and section loss are common on the stay-in-place forms in the widened portion of the structure. The corrugated metal pipe arches have significant corrosion, and have corroded away at several locations, exposing the concrete underside. The exposed concrete was generally in good condition, with a few minor cracks. Deterioration of these forms will not significantly affect the load carrying capacity of the concrete deck.

The widened portion of the deck appears to be in good condition with no notable deficiencies.

The twin-steel tube railings are in good condition with no apparent traffic impacts. Railing transition to the southeast approach railing is missing railing block outs and decreased post spacing. These were due to the proximity of the railing posts to the riprap, preventing additional posts from being installed at the proper distance away from the edge of the roadway.

### **Superstructure**

The original section of superstructure consists of six rolled steel beams and one steel channel (east exterior). The bottom flanges of the original portion were painted since the 2010 inspection. The interior beam bearings for this portion are covered with wood forms and likely encased in concrete making them inaccessible for inspection. The original beams bear on a masonry abutment, and the newer beams bear on reinforced concrete abutments. No significant signs of distress were noted at these beam ends.

The newer portion of the superstructure consists of six rolled steel beams supporting a conventional concrete deck with metal stay-in-place forms. The steel superstructure has been painted since the 2010 inspection. Square steel bars are welded across the bottom flanges of the beams at the new bridge railing supports. These welded bars and railing supports create fatigue prone details in the beam bottom flange. No cracks were observed at these welded details.

The steel beams in the widened portion of the bridge are in fair condition. Laminating corrosion noted on the west fascia beam has worsened since the 2013 inspection. Corrosion currently exists on both faces of the west fascia beam on the underside of the top flange, top of the bottom flange, and web. Section loss up to 1/8-inch deep was observed at several locations in the west fascia girder (**Photo 6**). The beam end at the north abutment for beam 1 also exhibits considerable laminating corrosion with up to 1/8-inch section loss to the beam web (**Photo 7**). The corrosion of the exterior beam is promoted by deck drainage passing over the edge of the bridge deck. A drip strip is absent from the edge of the deck allowing the drainage to run back to the beam, and the corrugated deck which is placed on top of the top flange allows the drainage to reach the inboard face of the beam.

The east fascia beam bearing is severely undermined due to heavy spalling of the south abutment bearing seat (**Photo 8**). Approximately 10% of the bearing area still exists at this location. Due to high water events at this structure, moderate amounts of debris exist around many of the bearings for the widened portion of the structure at the north abutment.

### **Substructure**

The widened portion of the substructure consists of reinforced concrete abutments while the original portion of the substructure consists of dry stacked block masonry (likely sandstone). The concrete for the abutments and wingwalls of the widened portion are generally in good condition, with no significant spalls, delaminations, or cracks noted. The concrete footings are exposed at both the north and south abutments with the north abutment being exposed along its entire length with some undercutting/fracturing of the supporting bedrock. This condition has not significantly changed from the 2013 inspection. No signs of rotation or settlement were noted in the concrete substructure units. See below for further description of scour conditions.

In the original portion of the substructure, many of the masonry blocks exhibit cracks and or missing stones. At the south abutment, 3/16-inch wide cracks exist under beams 8, 11, and 13 in the top course of masonry block. At the north abutment, one missing and one heavily cracked masonry block exists under beams 7 and 8 (**Photo 9**). Also at the north abutment, 1 1/8-inch maximum wide cracks exist in the second course of masonry blocks under beams 11 and 13 (**Photo 10**). The overall condition of the masonry blocks have not significantly changed since the 2012 inspection. No signs of rotation or settlement were noted within the masonry block substructure units.

Both abutments are supported on spread footings cast/laid on bedrock. Scour was noted along both abutments at the following locations: the west end of the north abutment is undermined laterally 14-inches maximum; the northwest wingwall is undermined laterally a maximum of 20-inches starting 5 feet west of the abutment breastwall; the north abutment under beam 8 is undermined a maximum of 8-inches laterally; the east corner of the south abutment is undermined laterally 12-inches maximum. These conditions have not changed significantly since the 2013 inspection and should be monitored during future inspections. No signs of rotation or settlement were noted during the inspection. Large diameter riprap was added at the southeast and northeast wingwalls prior to the 2011 inspection as scour countermeasures. The riprap is in place and appears to be functioning as designed.

Erosion was noted behind both the southeast and northwest wingwalls. The erosion to the embankment behind the northwest wingwall exposes the top five feet of the rear face of the wingwall. The erosion behind the southeast wingwall creates a steep slope which is 4-feet wide by 6-feet deep by 6-feet long (**Photo 11**). These conditions do not appear to have changed significantly since the 2013 inspection.

### **Channel**

The channel streambed is rocky and the banks are well vegetated both upstream and downstream of the structure. The channel alignment on this bridge is classified as poor. The channel was previously cutting into the embankment below and behind the southeast wingwall. Large riprap was installed at the northeast and southeast wingwalls help redirect the channel through the bridge. The riprap appears to be functioning as designed and is in good condition. The channel currently flows directly into the face of the north abutment, causing ongoing undermining of the footing. Undermining does not appear to have increased significantly

since the 2012 inspection. A pipe exists across the channel just upstream of the bridge. Large debris has become trapped against the pipe directing the flow further east (**Photo 12**).

### Approach

The approaches are paved with asphalt and are in poor condition. Approach pavement settlement exists in the north and south approach pavements adjacent to the abutments with significantly larger settlement noted in the north approach. A 1 1/2-inch maximum vertical offset with unsealed cracks were noted in the north approach pavement. This condition appears to have worsened by 1/4 inch in depth since the 2013 inspection (**Photo 13**). The settlement most likely is due to the excavation and installation of concrete pavement added at both ends of the bridge during the railing installation. This condition causes an extremely rough transition onto the bridge and increases the impact loads on the bridge. The unsealed cracks allow deck drainage to infiltrate the approach embankment, promoting further settlement of the pavement. Unsealed cracks are typical along the centerline in both asphalt pavements.

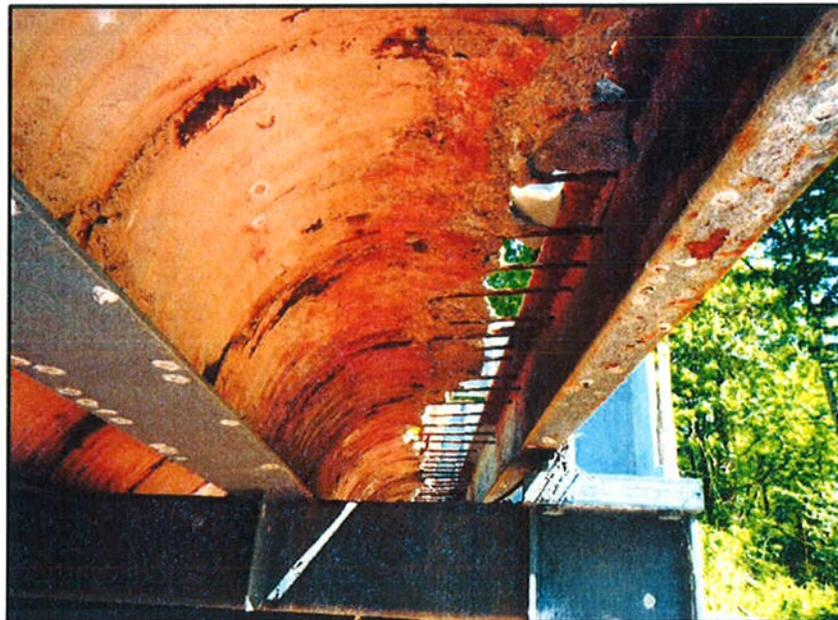
Newer steel guardrail with timber and steel posts exists at all four approach quadrants. Reflective tape exists at the ends of the oncoming guardrails; however, Z-board or chevron type signs are preferable to act as bridge end markers.



**Photo 3** – Looking north at the original portion of the deck in the northbound lane. Note the concrete wearing surface exhibits scaling and spalling in multiple locations.



**Photo 4** – Looking southeast at the east edge of the deck. Note a 26.5-foot long by 17-inch maximum wide hole exists in the deck edge with exposed and corroding reinforcing steel.



**Photo 5** – Looking up and north at the underside of the deck between beam 12 and the fascia channel beam along the east edge of the bridge. Note a 26-foot long by 13-inch wide hole exists through the deck.



**Photo 6** – Looking south along the exterior face of beam 1. Note the active laminating corrosion with section loss up to 1/8-inch deep on the flanges and web.



**Photo 7** – Looking north along the end of beam 1 at the north abutment. Note heavy laminating corrosion on the beam web with up to 1/8-inch section loss.



**Photo 8** – Looking southwest at the east fascia beam at the south abutment. Note severe undermining of the bearing due to heavy spalling of bearing seat. The structural tee bearing assembly is also heavily deteriorated with active section loss.



**Photo 9** – Looking north at the masonry block abutment under beam 8 at the north abutment. Note small missing block and heavily cracked and deteriorated block above.



**Photo 10** – Looking north at the second course of masonry block under beam 13. Note 1 1/8-inch wide crack in masonry block.



**Photo 11** – Looking down and northeast at the embankment behind the southeast wingwall. Note steep erosion to embankment.



**Photo 12** – Looking southeast at the upstream channel. Note pipe crosses channel. Also note debris build up along east end of pipe crossing.



**Photo 13** – Looking west at approach pavement adjacent to the north abutment. Note: cracking and settlement of approach pavement.

**RECOMMENDATIONS**

The following recommendations should be performed to maintain the current level of service for this structure for an extended period of time.

- Abrasively clean and paint the west fascia beam (beam 1).
- Repair the beam 13 bearing area at the south abutment. Remove all loose concrete, abrasively clean and paint the beam 13 channel, and place concrete up to the bottom flange of the channel. Dowel the new concrete into the existing masonry block.
- Patch areas of the northbound wearing surface which are spalled or delaminated. Monitor the newly placed and patched concrete wearing surface. When patching, remove all loose or unsound surfaces before placing new epoxy concrete. Due to the high probability of chloride contamination in the existing concrete, it is recommended that a full depth deck replacement be considered in lieu of patching. An alternative could be to replace the original structure with a pre-stressed concrete slab.
- Fill the eroded areas behind the southeast and northwest wingwalls with crushed aggregate and protect the aggregate with riprap.
- Remove debris from the north abutment beam seats.
- Remove the pipe crossing the channel upstream of the bridge and the ensnared drift.
- Add Z-board or chevron type bridge end markers at all four corners of the bridge.
- Continue to monitor the undermining of the abutments due to scour. Consider placing riprap along both abutments and removing streambed material to realign the stream under the bridge.
- Continue to monitor the cracked and missing masonry blocks at the abutments, especially under beams 7 and 8 at the north abutment. Consider doweling into the existing bedrock and masonry and pour concrete to encompass the area of distressed masonry.

We appreciate the opportunity to provide engineering services to you. If you have any questions or concerns, please feel free to contact this office.

Sincerely,



Dale E. Poorman, PE  
Project Engineer

copy: Mr. Mark E. Bernhardt, PE, Director of Facility Inspection  
File



5-23-2014

## STATE OF OHIO BRIDGE INSPECTION FIELD REPORT

 SFN not assigned  
 DIST 9

 Bridge Number not assigned  
 Feature Intersected Little Beaver Creek

 Year Built 1,930  
 Municipality 

	Qty.	condition state				cr	
		1	2	3	4	TR	
c1. Wearing Surface (SF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c2. Slab (SF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c3. Relief Joint (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c4. Embankment (LF) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c5. Guardrail (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
N36. Safety Features: Tr, Gr, Tm	36)B <input type="checkbox"/>	36)C <input type="checkbox"/>	36)D <input type="checkbox"/>				
c6. Approach Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c7.1 Floor/Slab (SF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c7.2 Edge of Floor/Slab (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c8. Wearing Surface (SF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c9. Curbs/Sidewalk (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c10. Median (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c11. Railing (LF)	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
N36. Safety Features: Rail	36)A <input checked="" type="checkbox"/>						
c12. Drainage (EA) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c13. Expansion Joint (LF) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
N58. Deck Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c14. Alignment (EA) <sup>ded</sup>	<input type="text"/>						
c15.1 Beams/Girders (LF)	<input type="text"/>						
c15.2 Slab (SF)	<input type="text"/>						
c16. Diaphragm/X-Frames (EA)	<input type="text"/>						
c17. Stringers (LF)	<input type="text"/>						
c18. Floorbeams (LF)	<input type="text"/>						
c19. Truss Verticals (EA)	<input type="text"/>						
c20. Truss Diagonals (EA)	<input type="text"/>						
c21. Truss Upper Chord (EA)	<input type="text"/>						
c22. Truss Lower Chord (EA)	<input type="text"/>						
c23. Truss Gusset Plate (EA) <sup>ded</sup>	<input type="text"/>						
c24. Lateral Bracing (EA)	<input type="text"/>						
c25. Sway Bracing (EA)	<input type="text"/>						
c26. Bearing Devices (EA) <sup>ded</sup>	<input type="text"/>						
c27. Arch (LF)	<input type="text"/>						
c28. Arch Column/Hanger (EA)	<input type="text"/>						
c29. Arch Spandrel Walls (LF)	<input type="text"/>						
c30. Prot. Coating System (LF) <sup>ded</sup>	<input type="text"/>						
c31. Pins/Hangers/Hinges (EA) <sup>ded</sup>	<input type="text"/>						
c32. Fatigue (LF) <sup>ded</sup>	<input type="text"/>						
N59. Superstructure Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c33. Abutment Walls (LF)	<input type="text"/>						
c34. Abutment Caps (LF)	<input type="text"/>						
c35. Abut. Colmns/Bents (EA)	<input type="text"/>						
c36. Pier Walls (LF)	<input type="text"/>						
c37. Pier Caps (LF)	<input type="text"/>						
c38. Pier Columns/Bents (EA)	<input type="text"/>						
c39. Backwalls (LF)	<input type="text"/>						
c40. Wingwalls (LF)	<input type="text"/>						
c42. Scour (LF) <sup>ded</sup>	<input type="text"/>						
c43. Slope Protection (LF) <sup>ded</sup>	<input type="text"/>						
N60. Substructure Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c44. General (LF)	<input type="text"/>						
c45. Alignment (LF) <sup>ded</sup>	<input type="text"/>						
c46. Shape (LF) <sup>ded</sup>	<input type="text"/>						
c47. Seams (LF) <sup>ded</sup>	<input type="text"/>						
c48. Headwall/Endwall (LF)	<input type="text"/>						
c49. Scour (LF) <sup>ded</sup>	<input type="text"/>						
c50. Abutments (LF)	<input type="text"/>						
N62. Culvert Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c51. Alignment (LF) <sup>ded</sup>	<input type="text"/>						
c52. Protection (LF) <sup>ded</sup>	<input type="text"/>						
c53. Hydraulic Opening (EA) <sup>ded</sup>	<input type="text"/>						
c54. Navigation Lights (EA) <sup>ded</sup>	<input type="text"/>						
N61. Channel Summary	(9-0)						<input type="text"/>

	Qty.	condition state				cr	
		1	2	3	4	TR	
c55. Signs (EA) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c56. Sign Supports (EA) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
c57. Utilities (LF) <sup>ded</sup>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
N59, 60 or 62 General Appraisal	(9-0)						<input type="text"/>
N41. Operating Status	(Open, Restricted, or Closed)						<input type="text"/>

Inspector Name	Reed Case
Inspection Date/Type	May 19, 2014 / RT FC UW SP
Reviewer Name	Dale Poorman
Review Date	Jun 12, 2014
PE Number (Insp or Rev)	52913

Key: "Qty" = Quantity necessary for Element Level inspection; "(LF)" = Linear Feet; "(SF)" = Square Feet; "(EA)" = Each or count; "CR" = 1, 2, 3 or 4 Condition Rating; "TR" = Transition Rating or weighted average of condition states; "ded" = dedicated or specific chart and guidance; "c" = condition prefix; "N" = NBIS rating

















